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Modeling magnetic saturation and saliency effects via Euler-Lagrange models with complex currents for three-phase permanent magnet machines

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Abstract:

Permanent magnet machines with both magnetic saturation and saliency effects can be directly described via Euler-Lagrangian formulation with complex currents. The Lagrangian is the sum of a mechanical kinetic energy and a magnetic Lagrangian. This second term is expressed in terms of rotor angle, complex stator and rotor magnetizing currents. Via simple modification of magnetic Lagrangian we derive a non-trivial dynamical model describing permanent-magnet machines with both saturation and saliency. We propose an experimental validation of such models on a customized torque machine of 1.2 kW. This first validation relies on injections of high frequency oscillations on the stator voltage. According to the proposed saturation model, the resulting amplitudes of the current-ripples is an increasing function of the current offset. Such dependance is effectively observed experimentally and confirmed by simulations.

Keywords: Lagrangian with complex coordinates, magnetic saturation, saliency, permanent-magnet machine, high frequency injection.

1. INTRODUCTION

Modeling permanent magnet machines with magnitude saturation is not a straightforward task and could lead to complicated developments when a detailed physical description is included (see, e.g., Chiasson [2005], Boldea and Nasar [2002]). Even if such effects are not dominant they play an important role at low speed and/or high torque and stator current. The contributions of this communication are as follows :

- simple models (see (10)), including simultaneously saturation and saliency and extending directly usual models used in the literature.
- A first experimental validation of such magnetic saturation models for a 1.2 kW machine. It relies on high frequency voltage injection and on the measures of the resulting ripples on the stator current.

We exploit here Basic et al. [2009] that proposes an extension to complex electrical variable of Lagrangian modeling of electrical machines.

In section 2 we recall the simplest model of a permanent magnet machine and its Euler-Lagrange formulation based on the two scalar components of the complex stator current. We recall the complexification procedure and explain how to derive the Euler-Lagrange equations directly with

complex stator current. Then we provide the general form of physically consistent models (equation (5)). Finally we obtain, just by simple modification of the magnetic Lagrangian, physically consistent models with magnetic saturation and saliency effects (equation (10)). We also derive the associated magnetic energies of such non-linear magnetic models. In section 3, we propose a simple experimental validation of the nonlinear magnetic model introduced in previous section (equation (10) with λ given by (12)). The validation is based on high frequency voltage injection and measurement of the associated current-ripples. Perturbations techniques provide analytic expressions of these ripples, expressions depending on the level of permanent currents. Experimental data on a 1.2 kW machine confirm the fact that the current ripples are an increasing function of the current static offset. These experimental data also confirm that the injected frequencies are not too high (less than a few kHz) and that the main flux distribution is not altered by skin effects in magnets and laminations and that magnetic core losses could be neglected here. Simulations confirm that such dependance is typical of such magnetic saturations.

2. EULER-LAGRANGE MODELLING WITH COMPLEX CURRENTS AND VOLTAGES

2.1 The usual model and its Euler-Lagrange formulation

In the (α, β) frame (total power invariant transformation), the dynamic equations read (see, e.g., Chiasson [2005], Leonhard [1985]):

$$\begin{cases} \frac{d}{dt} (J\dot{\theta}) = n_p \Im \left((\bar{\phi} e^{jn_p\theta})^* \iota_s \right) - \tau_L \\ \frac{d}{dt} (\lambda \iota_s + \bar{\phi} e^{jn_p\theta}) = u_s - R_s \iota_s \end{cases} \quad (1)$$

where

- $*$ stands for complex-conjugation, $j = \sqrt{-1}$ and n_p is the number of pairs of poles.
- θ is the rotor mechanical angle, J and τ_L are the inertia and load torque, respectively.
- $\iota_s \in \mathbb{C}$ is the stator current, $u_s \in \mathbb{C}$ the stator voltage.
- $\lambda = (L_d + L_q)/2$ with inductances $L_d = L_q > 0$ (no saliency here).
- The stator flux is $\phi_s = \lambda \iota_s + \bar{\phi} e^{jn_p\theta}$ with the constant $\bar{\phi} > 0$ representing to the rotor flux due to permanent magnets.

It is well known that (1) derives from a variational principle (see, e.g., Ortega et al. [1998]) and thus can be written as Euler-Lagrange equations with source terms corresponding to energy exchange with the environment. Consider the additional complex variable $q_s \in \mathbb{C}$ defined by $\frac{d}{dt} q_s = \iota_s$. The Lagrangian associated to this system is the sum of the mechanical kinetic Lagrangian \mathcal{L}_c and magnetic one \mathcal{L}_m defined as follows:

$$\mathcal{L}_c = \frac{J}{2} \dot{\theta}^2, \quad \mathcal{L}_m = \frac{\lambda}{2} |\iota_s + I_m e^{jn_p\theta}|^2 \quad (2)$$

where $I_m = \bar{\phi}/\lambda > 0$ is the permanent magnetizing current.

Take the complete Lagrangian $\mathcal{L} = \mathcal{L}_c + \mathcal{L}_m$ as a real function of the generalized coordinates $q = (\theta, q_{s\alpha}, q_{s\beta})$ and generalized velocities $\dot{q} = (\dot{\theta}, \iota_{s\alpha}, \iota_{s\beta})$:

$$\mathcal{L}(q, \dot{q}) = \frac{J}{2} \dot{\theta}^2 + \frac{\lambda}{2} ((\iota_{s\alpha} + I_m \cos n_p\theta)^2 + (\iota_{s\beta} + I_m \sin n_p\theta)^2) \quad (3)$$

with $q_s = q_{s\alpha} + jq_{s\beta}$, ($q_{s\alpha}$ and $q_{s\beta}$ real) and $\dot{q}_s = \iota_s = \iota_{s\alpha} + j\iota_{s\beta}$, ($\iota_{s\alpha}$ and $\iota_{s\beta}$ real). Then the mechanical equation in (1) reads

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{\theta}} \right) - \frac{\partial \mathcal{L}}{\partial \theta} = -\tau_L$$

where $-\tau_L$ corresponds to the energy exchange through the mechanical load torque. Similarly, the real part of complex and electrical equation in (1) reads

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_{s\alpha}} \right) - \frac{\partial \mathcal{L}}{\partial q_{s\alpha}} = u_{s\alpha} - R_s \iota_{s\alpha}$$

and its imaginary part

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_{s\beta}} \right) - \frac{\partial \mathcal{L}}{\partial q_{s\beta}} = u_{s\beta} - R_s \iota_{s\beta}$$

since $\frac{\partial \mathcal{L}}{\partial q_{s\alpha}} = \frac{\partial \mathcal{L}}{\partial q_{s\beta}} = 0$ and $\dot{q}_s = \iota_s$. The energy exchanges here are due to the power supply through the voltage u_s

and also to dissipation and irreversible phenomena due to stator resistance represented by the Ohm law $-R_s \iota_s$.

2.2 Euler-Lagrange equation with complex current

The drawback of such Lagrangian formulation is that we have to split into real and imaginary parts the generalized coordinates associated to q_s and $\dot{q}_s = \iota_s$. We do not preserve the elegant formulation of the electrical part through complex variables and equations. We will show here that it is still possible to extend such complex formulation to the Euler-Lagrange equations. It seems that it has never been used for electrical machines. We recall here below the principle of such complexification (usual in quantum electro-dynamics) and then applied it to the above Euler-Lagrange formulation.

Consider a Lagrangian system with two generalized coordinates q_1 and q_2 corresponding to a point $q = q_1 + jq_2$ in the complex plane ($j = \sqrt{-1}$). The Lagrangian $\mathcal{L}(q_1, q_2, \dot{q}_1, \dot{q}_2)$ is a real function and the Euler-Lagrange equations are

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_1} \right) - \frac{\partial \mathcal{L}}{\partial q_1} = 0, \quad \frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_2} \right) - \frac{\partial \mathcal{L}}{\partial q_2} = 0.$$

Using the complex notation q , we have $q_1 = \frac{q+q^*}{2}$ and $q_2 = \frac{q-q^*}{2j}$, thus \mathcal{L} is also a function of $q, q^*, \frac{d}{dt}q$ and $\frac{d}{dt}q^*$:

$$\tilde{\mathcal{L}}(q, q^*, \dot{q}, \dot{q}^*) \equiv \mathcal{L} \left(\frac{q+q^*}{2}, \frac{q-q^*}{2j}, \frac{\dot{q}+\dot{q}^*}{2}, \frac{\dot{q}-\dot{q}^*}{2j} \right).$$

The above identity defines $\tilde{\mathcal{L}}$ as a function of the 4 complex independent variables $(q, q^*, \dot{q}, \dot{q}^*)$. Simple computations show that

$$2 \frac{\partial \tilde{\mathcal{L}}}{\partial q} = \frac{\partial \mathcal{L}}{\partial q_1} - j \frac{\partial \mathcal{L}}{\partial q_2}, \quad 2 \frac{\partial \tilde{\mathcal{L}}}{\partial q^*} = \frac{\partial \mathcal{L}}{\partial q_1} + j \frac{\partial \mathcal{L}}{\partial q_2}$$

and similarly

$$2 \frac{\partial \tilde{\mathcal{L}}}{\partial \dot{q}} = \frac{\partial \mathcal{L}}{\partial \dot{q}_1} - j \frac{\partial \mathcal{L}}{\partial \dot{q}_2}, \quad 2 \frac{\partial \tilde{\mathcal{L}}}{\partial \dot{q}^*} = \frac{\partial \mathcal{L}}{\partial \dot{q}_1} + j \frac{\partial \mathcal{L}}{\partial \dot{q}_2}.$$

Thus with this complex notation, we can gather the two real Euler-Lagrange equations into a single complex one

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_1} + j \frac{\partial \mathcal{L}}{\partial \dot{q}_2} \right) = \frac{\partial \mathcal{L}}{\partial q_1} + j \frac{\partial \mathcal{L}}{\partial q_2}$$

that reads now simply

$$\frac{d}{dt} \left(2 \frac{\partial \tilde{\mathcal{L}}}{\partial \dot{q}^*} \right) - 2 \frac{\partial \tilde{\mathcal{L}}}{\partial q^*} = 0.$$

Let us apply this complexification procedure to the Lagrangian $\mathcal{L}(\theta, q_{s\alpha}, q_{s\beta}, \dot{\theta}, \dot{q}_{s\alpha}, \dot{q}_{s\beta})$ defined in (3). The complexification process only applies to q_s and $\dot{q}_s = \iota_s$ by considering \mathcal{L} as a function of $(\theta, q_s, q_s^*, \dot{\theta}, \iota_s, \iota_s^*)$:

$$\mathcal{L}(\theta, \dot{\theta}, \iota_s, \iota_s^*) = \frac{J}{2} \dot{\theta}^2 + \frac{\lambda}{2} (\iota_s + I_m e^{jn_p\theta}) (\iota_s^* + I_m e^{-jn_p\theta}).$$

Then the usual equations (1) read

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{\theta}} \right) = \frac{\partial \mathcal{L}}{\partial \theta} - \tau_L, \quad 2 \frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{\iota}_s^*} \right) = u_s - R_s \iota_s$$

since $\frac{\partial \mathcal{L}}{\partial q_s^*} = 0$ and $\frac{\partial \mathcal{L}}{\partial \dot{q}_s^*} = \frac{\partial \mathcal{L}}{\partial \dot{\iota}_s^*}$.

More generally, the magnetic Lagrangian \mathcal{L}_m is a real value function of θ, ι_s and ι_s^* that is $\frac{2\pi}{n_p}$ periodic versus θ . Thus

any Lagrangian \mathcal{L}_{PM} representing a 3-phases permanent magnet machine admits the following form

$$\mathcal{L}_{\text{PM}} = \frac{J}{2} \dot{\theta}^2 + \mathcal{L}_m(\theta, \iota_s, \iota_s^*) \quad (4)$$

Consequently, any model (with saliency, saturation, space-harmonics, ...) of permanent magnet machines admits the following structure:

$$\frac{d}{dt} (J\dot{\theta}) = \frac{\partial \mathcal{L}_m}{\partial \theta} - \tau_L, \quad \frac{d}{dt} \left(2 \frac{\partial \mathcal{L}_m}{\partial \iota_s^*} \right) = u_s - R_s \iota_s \quad (5)$$

and we recover the usual equation with $\phi_s = 2 \frac{\partial \mathcal{L}_m}{\partial \iota_s^*}$ corresponding to the stator flux. The model considered here above derives from a magnetic Lagrangian of the form

$$\mathcal{L}_m = \frac{\lambda}{2} |\iota_s + I_m e^{j n_p \theta}|^2$$

with λ and I_m are two positive parameters.

Many other formulations of \mathcal{L}_m are possible and depend on particular modeling issues. Usually, the dominant part of \mathcal{L}_m will be of the form $\frac{\bar{\lambda}}{2} |\iota_s + I_m e^{j n_p \theta}|^2$ ($\bar{\lambda}$, I_m positive constants) to which is added corrections terms that are "small" scalar functions of $(\theta, \iota_s, \iota_s^*)$.

The magnetic energy H_m does not coincides with \mathcal{L}_m . It is given by the Hamiltonian, H_m , defined via a Legendre transform on \mathcal{L}_m . Following the complex formulation used in quantum electro-dynamics (see [Cohen-Tannoudji et al., 1989, page 88, equation (A.30)]) we have:

$$H_m(\theta, \iota_s, \iota_s^*) = \iota_s \frac{\partial \mathcal{L}_m}{\partial \iota_s}(\theta, \iota_s, \iota_s^*) + \iota_s^* \frac{\partial \mathcal{L}_m}{\partial \iota_s^*}(\theta, \iota_s, \iota_s^*) - \mathcal{L}_m(\theta, \iota_s, \iota_s^*). \quad (6)$$

Notice that, when $\mathcal{L}_m = \frac{\lambda}{2} |\iota_s + I_m e^{j n_p \theta}|^2$ with λ and I_m constant, we get $H_m = \frac{\lambda}{2} (|\iota_s|^2 - I_m^2)$ and we recover the usual magnetic energy $\frac{\lambda}{2} |\iota_s|^2$ up to the constant magnetizing energy $\frac{\lambda}{2} I_m^2$. In next two sub-sections, we introduce some modifications to this standard Lagrangian \mathcal{L}_m to take into account saliency and saturation effects and derive the corresponding magnetic energy H_m .

2.3 Saliency models

Adding to \mathcal{L}_m the correction $-\frac{\mu}{2} \Re(\iota_s^2 e^{-2j n_p \theta})$ with $|\mu| < \lambda$ (\Re means real part) provides a simple way to represent saliency phenomena while the dominant part of the magnetic Lagrangian (and thus of the dynamics) remains attached to $\frac{\lambda}{2} |\iota_s + I_m e^{j n_p \theta}|^2$. With magnetic Lagrangian of the form

$$\mathcal{L}_m = \frac{\lambda}{2} (\iota_s + I_m e^{j n_p \theta}) (\iota_s^* + I_m e^{-j n_p \theta}) - \frac{\mu}{4} \left((\iota_s^* e^{j n_p \theta})^2 + (\iota_s e^{-j n_p \theta})^2 \right) \quad (7)$$

where $\lambda = (L_d + L_q)/2$ and $\mu = (L_q - L_d)/2$ (inductances $L_d > 0$ and $L_q > 0$), equations (5) become ($\lambda I_m = \bar{\phi}$)

$$\begin{cases} \frac{d}{dt} (J\dot{\theta}) = n_p \Im((\lambda \iota_s^* + \bar{\phi} e^{-j n_p \theta} - \mu \iota_s e^{-2j n_p \theta}) \iota_s) - \tau_L \\ \frac{d}{dt} (\lambda \iota_s + \bar{\phi} e^{j n_p \theta} - \mu \iota_s^* e^{2j n_p \theta}) = u_s - R_s \iota_s \end{cases} \quad (8)$$

and we recover the usual model with saliency effect. In this case the magnetic energy $H_m = \iota_s \frac{\partial \mathcal{L}_m}{\partial \iota_s} + \iota_s^* \frac{\partial \mathcal{L}_m}{\partial \iota_s^*} - \mathcal{L}_m$ is given by:

$$H_m = \frac{\lambda}{2} (|\iota_s|^2 - I_m^2) - \frac{\mu}{4} \left((\iota_s^* e^{j n_p \theta})^2 + (\iota_s e^{-j n_p \theta})^2 \right)$$

2.4 Saturation and saliency models

We can also take into account magnetic saturation effects, i.e., the fact that inductances depend on the currents. Let us assume that only the mean inductance λ in (7) depends on the modulus of $\iota_s + I_m e^{j n_p \theta}$ and that μ remains constant:

$$\lambda = \lambda(|\iota_s + I_m e^{j n_p \theta}|) = \lambda \left(\sqrt{(\iota_s + I_m e^{j n_p \theta})(\iota_s^* + I_m e^{-j n_p \theta})} \right).$$

The derivative of λ versus the modulus of $\iota_s + I_m e^{j n_p \theta}$ is denoted by λ' . The magnetic Lagrangian now reads

$$\mathcal{L}_m = \frac{\lambda(|\iota_s + I_m e^{j n_p \theta}|)}{2} |\iota_s + I_m e^{j n_p \theta}|^2 - \frac{\mu}{4} \left((\iota_s^* e^{j n_p \theta})^2 + (\iota_s e^{-j n_p \theta})^2 \right). \quad (9)$$

The dynamics is given by (5) with such \mathcal{L}_m . Since

$$\frac{\partial \lambda}{\partial \theta} = n_p \frac{\Im(I_m e^{-j n_p \theta} \iota_s)}{|\iota_s + I_m e^{j n_p \theta}|} \lambda', \quad \frac{\partial \lambda}{\partial \iota_s^*} = \frac{\iota_s + I_m e^{j n_p \theta}}{2|\iota_s + I_m e^{j n_p \theta}|} \lambda'$$

we get the following model structure with both saliency and magnetic saturation effects:

$$\begin{cases} \frac{d}{dt} (J\dot{\theta}) = n_p \Im \left((\Lambda (\iota_s^* + I_m e^{-j n_p \theta}) - \mu \iota_s e^{-2j n_p \theta}) \iota_s \right) - \tau_L \\ \frac{d}{dt} (\Lambda (\iota_s + I_m e^{j n_p \theta}) - \mu \iota_s^* e^{2j n_p \theta}) = u_s - R_s \iota_s \end{cases} \quad (10)$$

where $\Lambda = \lambda + \frac{|\iota_s + I_m e^{j n_p \theta}|}{2} \lambda'$. It is interesting to compute the magnetic energy H_m from general formula (6):

$$H_m = \frac{\lambda + |\iota_s + I_m e^{j n_p \theta}| \lambda'}{2} |\iota_s|^2 + \frac{|\iota_s + I_m e^{j n_p \theta}| \lambda'}{2} I_m \Re(\iota_s e^{-j n_p \theta}) - \frac{\lambda}{2} I_m^2 - \frac{\mu}{4} \left((\iota_s^* e^{j n_p \theta})^2 + (\iota_s e^{-j n_p \theta})^2 \right). \quad (11)$$

Such magnetic energy formulae are not straightforward but there are a direct consequence of such variational formulation of the dynamics and its setting with complex electrical variables.

We will assume now and in the sequel that λ admits the following parametric form:

$$\lambda(\iota) = 2\lambda_0 \frac{\sqrt{1 + \left(\frac{\iota}{\iota_{\text{sat}}}\right)^2} - 1}{\left(\frac{\iota}{\iota_{\text{sat}}}\right)^2} \quad (12)$$

with two positive parameters $\lambda_0 > 0$ and $\iota_{\text{sat}} > 0$. It yields for Λ to the following simple expression:

$$\Lambda(\iota) = \frac{\lambda_0}{\sqrt{1 + (\iota/\iota_{\text{sat}})^2}} \quad (13)$$

Thus with (13), the model (10) describes simultaneously saliency and saturation with 4 physically meaning positive parameters μ , λ_0 , I_m and ι_{sat} . We will see that such expressions are well adapted for saturation modelling.

3. A FIRST EXPERIMENTAL VALIDATION

3.1 Description of the test

Assume that the rotor is blocked via a mechanical brake at position $\theta = 0$. Consider the following voltage inputs

$$u_s(t) = u_s^r + u_s^a f(\Omega t) \quad (14)$$

where

- the complex quantities u_s^r and u_s^a are constant;
- the real-value function $\gamma \mapsto f(\gamma)$ is 2π periodic with a zero mean, $\int_0^{2\pi} f(\gamma) d\gamma = 0$;
- the pulsation Ω is large (typically around 1kHz).

In the sequel F denotes the primitive of f , $\frac{dF}{d\gamma} = f$, that admits a zero mean, $\int_0^{2\pi} F(\gamma) d\gamma = 0$. Then the electrical dynamics obey to the following differential implicit equation:

$$\frac{d}{dt} (\Lambda (\iota_s + I_m) - \mu \iota_s^*) = u_s^r + u_s^a f(\Omega t) - R_s \iota_s \quad (15)$$

where Λ is given by (13). Set $\iota_s^r = u_s^r / R_s$ its asymptotically and hyperbolically stable solution when $u_s^a = 0$. For Ω large enough, the solution of (15) converges towards a small periodic orbits around ι_s^r : $\iota_s(t) = \iota_s^r + \delta \iota_s(\Omega t)$ where the complex-value function $\gamma \mapsto \delta \iota_s(\gamma)$ is 2π -periodic with zero mean. $\delta \iota_s(\Omega t)$ corresponds to the so-called current ripples resulting from the high frequency injection $u_s^a f(\Omega t)$. The above statement can be rigorously proved by averaging theorem (see, e.g., [Guckenheimer and Holmes, 1983, theorem 4.1.1, page 168]) since the unperturbed system is asymptotically stable (for $|\mu|$ small enough, it is in fact a strict contraction in the sense of Lohmiller and Slotine [1998] for the Euclidian metric on the stator flux in \mathbb{C}).

Standard asymptotics for Ω tending to $+\infty$ show that the current ripples $\delta \iota_s$ satisfy to the following complex equation:

$$\begin{aligned} \left(\Lambda + \frac{|\iota_s^r + I_m| \Lambda'}{2} \right) \delta \iota_s + \left(\frac{(\iota_s^r + I_m)^2 \Lambda'}{2 |\iota_s^r + I_m|} - \mu \right) \delta \iota_s^* \\ = \frac{u_s^a}{\Omega} F(\Omega t) + O\left(\frac{|u_s^a|^2}{\Omega^2}\right) \end{aligned}$$

where Λ and its ι -derivative Λ' are evaluated at $\iota = |\iota_s + I_m|$. Assume u_s^r real, then $\iota_s^r = u_s^r / R_s$ is real too and the above formulae simplify a little

$$\begin{aligned} \left(\Lambda + \frac{|\iota_s^r + I_m| \Lambda'}{2} \right) \delta \iota_s + \left(\frac{|\iota_s^r + I_m| \Lambda'}{2} - \mu \right) \delta \iota_s^* \\ = \frac{u_s^a}{\Omega} F(\Omega t) + O\left(\frac{|u_s^a|^2}{\Omega^2}\right). \quad (16) \end{aligned}$$

For u_s^a real, $\delta \iota_s$ is real and given by:

$$(\Lambda + |\iota_s^r + I_m| \Lambda' - \mu) \delta \iota_s = \frac{u_s^a}{\Omega} F(\Omega t) + O\left(\frac{|u_s^a|^2}{\Omega^2}\right).$$

Using (13), we have

$$\left(\frac{\lambda_0}{\left(1 + \frac{(\iota_s^r + I_m)^2}{\iota_{\text{sat}}^2}\right)^{\text{vsat}}} - \mu \right) \delta \iota_s \approx \frac{u_s^a}{\Omega} F(\Omega t). \quad (17)$$

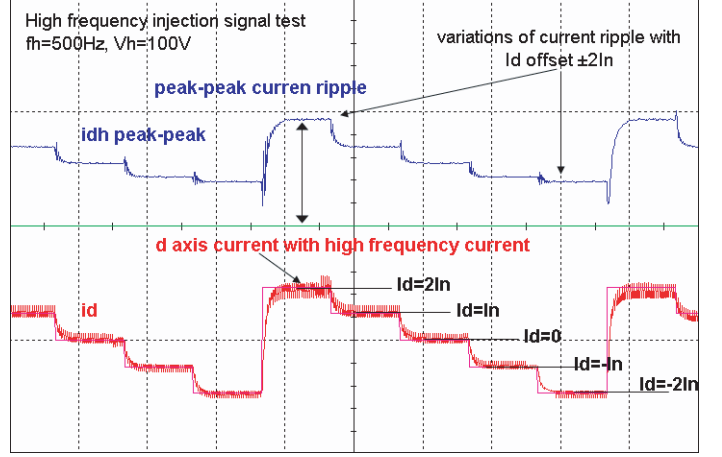


Fig. 1. Experimental data. The blue curve corresponds to the amplitudes of the current-ripples (obtained via a simple PLL-filter) ; the red curve to the current measures ι_s (d -axis aligned with the rotor $\theta = 0$); we observe an increasing dependance of the ripples versus the current offset ι_s^r .

We should observe experimentally that, for the same high frequency voltage excitation, the amplitudes of the current ripples depend on the current offset ι_s^r .

3.2 Simulation vs experimental results for a 1.2 kW machine

We take a permanent magnet synchronous motor of 1.2 kW from the manufacturer Bernecker+Rainer, Industrie-Elektronik Ges. M.b.h, Eggelsberg, Austria (reference: 8YS-H0004R0.029-0). For this motor, we have $n_p = 6$, the nominal current $I_n = 2.4$ A and $R_s = 6.7$ Ohms. The magnetizing current I_m is around $2.6I_n$, the saturation current ι_{sat} is about $5I_n$, the main inductance λ_0 is equal to 92.6mH and the saliency μ almost vanishes. Thus, for this motor and according to (17), the amplitude of the current-ripples should be an increasing function of ι_s^r when $\iota_s^r + I_m > 0$.

The parameters of the high frequency voltage injection are $\Omega/2\pi = 500$ Hz, $|u_s^a| = 100$ V and $f(\gamma) = \text{sign}(\sin(\gamma))$.

We use five real values for the constant voltage injections u_s^r leading to five levels for $\iota_s^r \in \{2I_n, I_n, 0, -I_n, -2I_n\}$. For each value of ι_s^r , we estimate the amplitude of the current-ripples via a simple PLL-filter. The experimental results are reported on figure 1.

We observe, as predicted via the theory, that this amplitude decreases when ι_s^r decreases. The simulation results are shown in figure 2. This dependance cannot be explained via the standard model (8) with linear inductances and results from non-negligible magnetic saturation effects. Indeed, the simulation results in figure 3, obtained with linear inductances, show constant ripples independently of the total magnetizing current $|\iota_s + I_m|$. In the case of the standard model, we define the value of the inductance λ by

$$\lambda = \frac{\lambda_0}{\sqrt{1 + (I_m / \iota_{\text{sat}})^2}}$$

equals to 82.2mH.

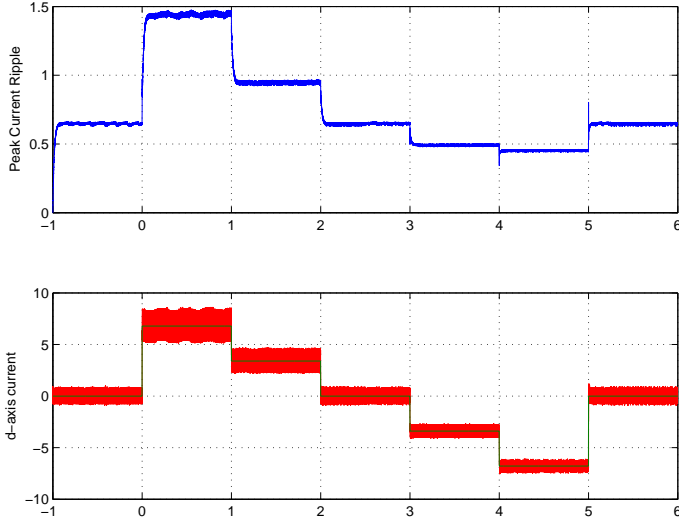


Fig. 2. Simulation data with saturation model. The first curve (up) corresponds to the amplitudes of the current-ripples ; the red curve to the current measures i_s (d -axis aligned with the rotor $\theta = 0$); as predicted by theory, we observe in simulation an increasing dependance of the ripples versus the current offset i_s^r .

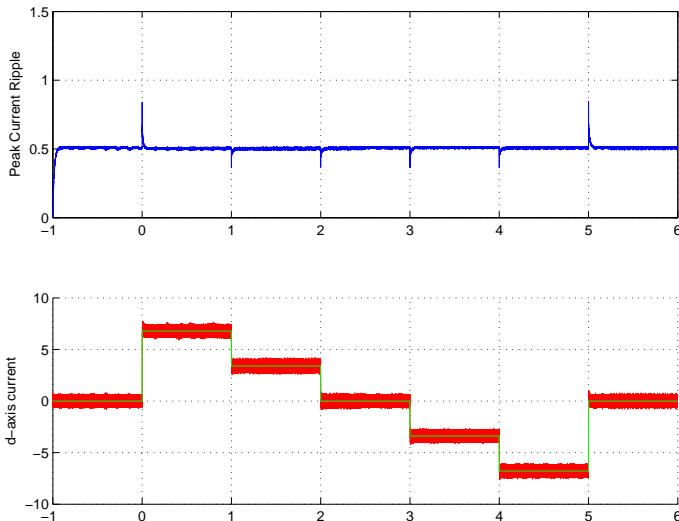


Fig. 3. Simulation data with standard model without saturation. The first curve (up) corresponds to the amplitudes of the current-ripples ; the red curve to the current measures i_s (d -axis aligned with the rotor $\theta = 0$); as predicted by theory, we observe in simulation that ripples stay constant independently of the current offset i_s^r .

We chose here a particular context with $\theta = 0$ in order to get the simplest computation and experimental test of such modelling. The above developments remain also valid when θ is no more fixed to 0 and when saliency (level and position) induced by saturation depends on the load torque.

4. CONCLUSION

The saturation models (10) for permanent-magnet machine with λ given by (12) are based on variational prin-

ciples and Lagrangian formulation of the dynamics. Experimental data provide a first validation of such modelling procedures that preserve the physical insight while maintaining a synthetic view without describing all the technological and material details.

More complete validations could be done: at non zero rotor velocity, the proposed computations of the current ripples are still possible since they are obtained via usual perturbations techniques. More complex models can be developed with μ depending also on $|i_s + I_m|$. Such models can also be used for control purposes: adaptation of usual control schemes to take into account saturation effects are under study.

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